

The logo for EDICON 2018, featuring the text 'EDI' in black and 'CON' in white on a blue background, with '2018' in red below it.

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Electronic Design Innovation
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The event details, including the dates 'October 17-19 2018' and the location 'Santa Clara Convention Center, Santa Clara, CA'.

October 17-19 2018
Santa Clara Convention Center
Santa Clara, CA

High speed/mm-wave measurement-based model development: uncertainties and model sensitivities

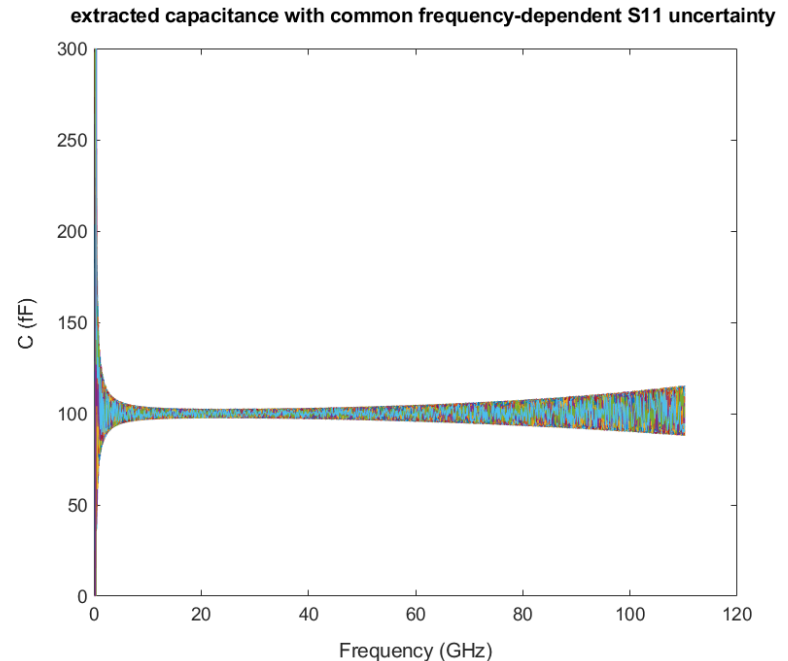
J. Martens

The Anritsu logo, consisting of the word 'Anritsu' in a bold, green, sans-serif font, with the tagline 'envision : ensure' in a smaller, grey, sans-serif font below it.

Anritsu
envision : ensure

Introduction/motivation

- Measurement-based model extraction does not get easier at mm-wave frequencies
 - Uncertainties in measurement increase
 - Extraction processes can have sensitive zones
- A better understanding of the parameter space (focus on network analyzer measurements) and behaviors of the extractions can perhaps improve results.

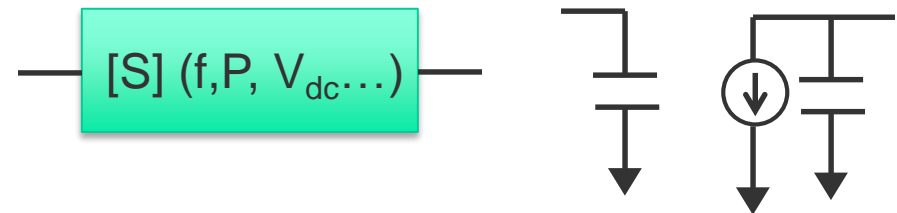
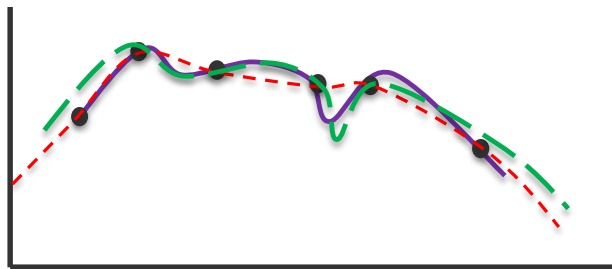


Outline

- Background
- Measurement uncertainties
 - Instrumentation-related terms
 - Calibration and de-embedding
 - Quasi-linear measurements: source purity, power accuracy
 - Correlation
- Extraction
 - Common conversions for compact models
 - Correlation implications
 - Behavioral extractions
- Uncertainty and extraction overlap
 - Mitigation possibilities
 - Asymptotic choices

Background 1

- While EM and multi-physics models can satisfy many needs, measurement-based models are still needed
 - *To evaluate/characterize new processes*
 - *Use for extended range applications*
 - *In more nonlinear realms*
- The models may be compact/circuit-based or may be behavioral. The extraction interacts with underlying data in different ways.

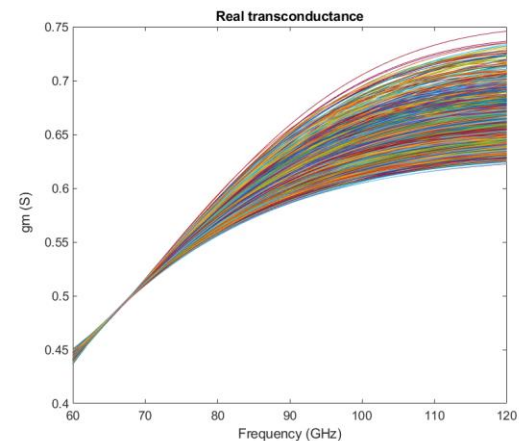
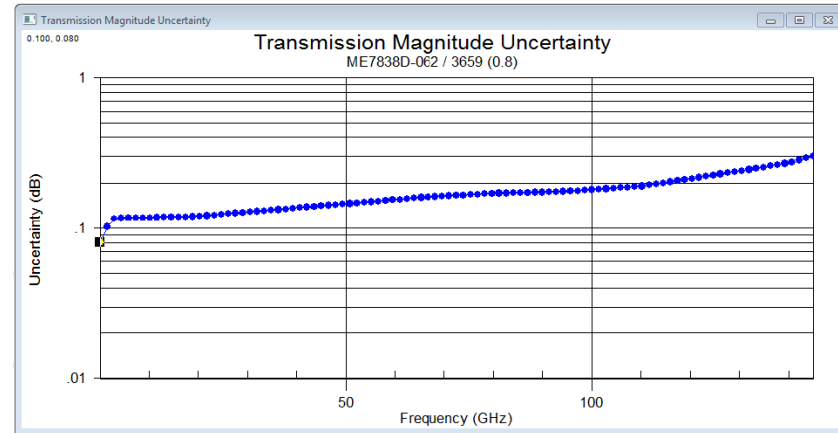


Mm-wave models may be changing more rapidly with many input parameters

Background 2

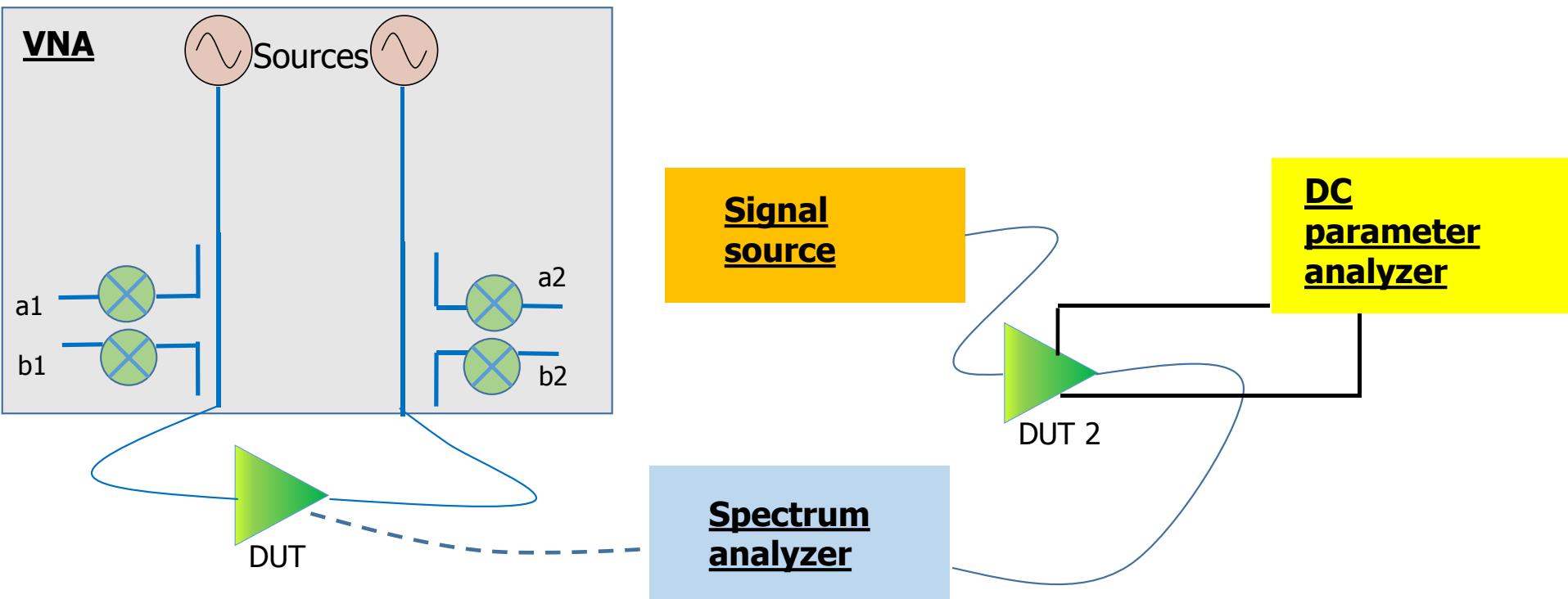
- At higher frequencies, measurement uncertainties generally increase.
 - Higher conversion loss and lower power → more noise issues.
 - Degrading repeatability
 - Shorter wavelength → more phase issues from minor physical problems

- Very large model uncertainties have been the outcome in some cases.



Measurement configurations

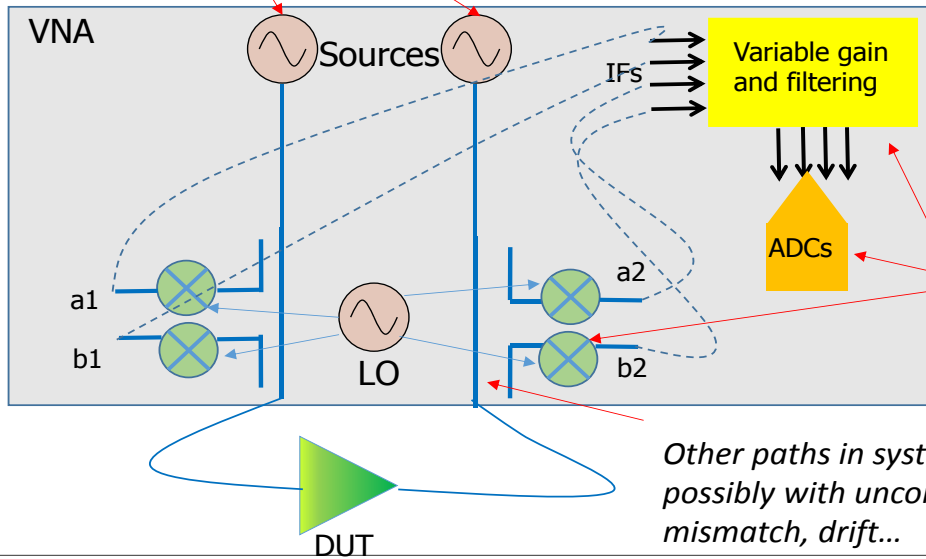
- Many tools may be employed but we will focus on the VNA effects. The uncertainty parameters for the other RF tools are often a subset.



Measurement configurations II

- VNA uncertainty elements: repeatability, nonlinearities, noise, drift, correction/de-embedding limitations...

Sources possibly with noise, harmonics, nonlinear output match



Nonlinearities usually do not get worse at higher frequencies (until near-THz), but the other elements all do.

Receivers possibly with noise, linearity, drift

Other paths in system possibly with uncorrected mismatch, drift...

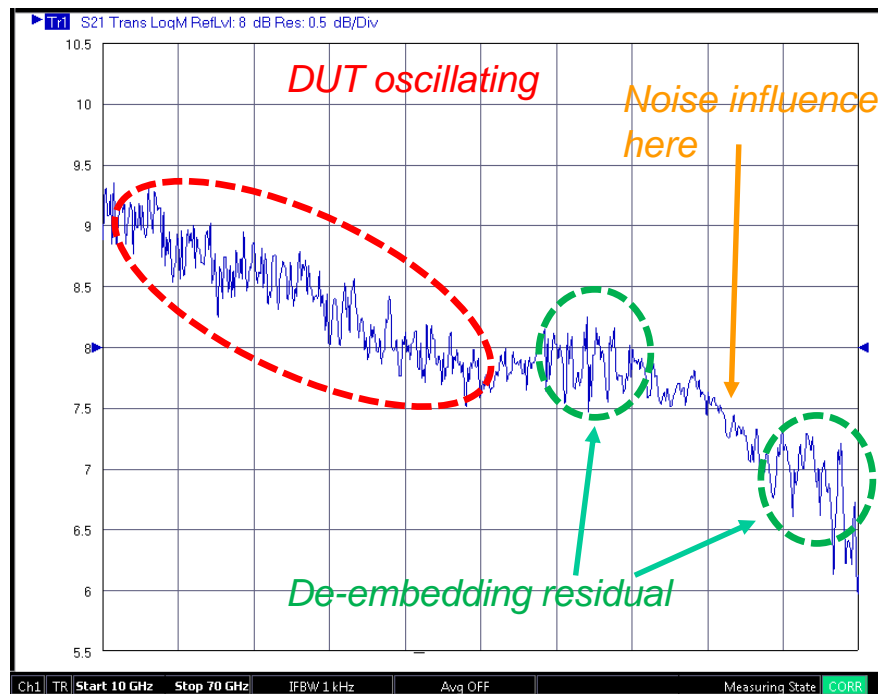
Measurement configurations III

The physical DUT environment has a strong influence on net uncertainty:

- Waveguide/coax: repeatability (and not direct for device modeling)
- Fixtured: repeatability, how good are the de-embedding structures?, crosstalk
- On-wafer: contact repeatability, de-embedding limits, crosstalk, multi-mode propagation

Mechanisms: Noise

- Is it really noise?
 - If so, which mechanism?
 - This actually matters since the dependencies are not the same.

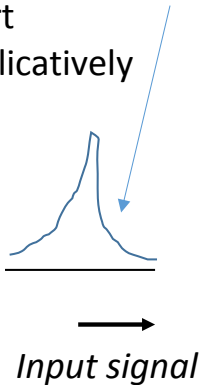


- In most measurements, there is an additive noise component (not dependent on input signal amplitude) and a multiplicative one.

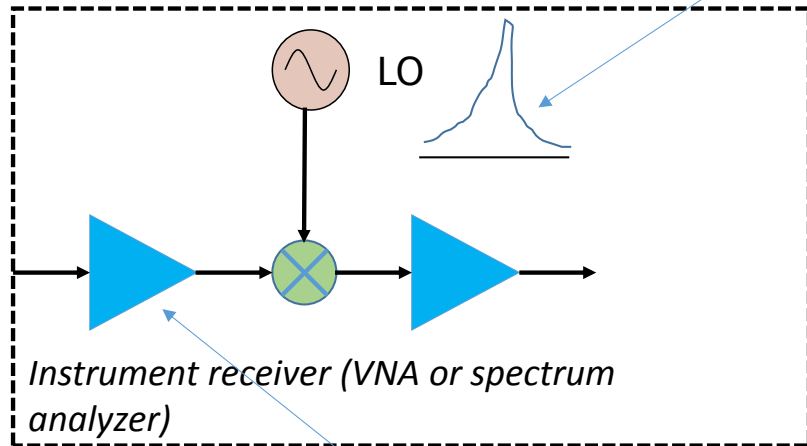
Mechanisms: Noise (2)

- The signal and LO-based noise contributors can be complicated. Knowing the weights can enable an optimal signal plan...

Input noise skirts can convert multiplicatively



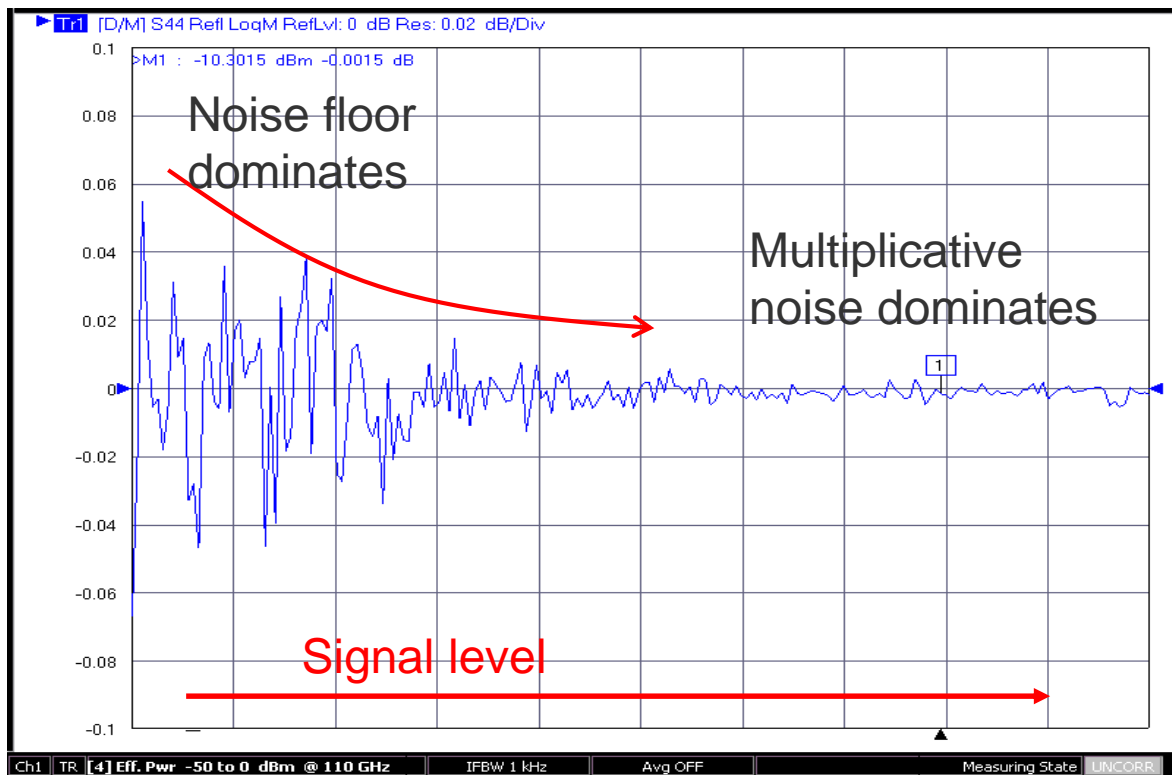
LO noise skirts can have an additive and a multiplicative element



Amplifier noise is usually additive

Mechanisms: Noise (3)

- At low levels, additive noise dominates so increasing the desired signal level helps (in dB terms).
- At higher levels, the noise and signal increase at the same relative rate
- Some cancellation does occur in a ratioed measurement at high levels.



Mechanisms: Repeatability

- Environment matters
 - Coax: Repeatability levels ~ -50 to -60 dB through 145 GHz (well-maintained connectors). $\ll 0.1$ dB usually.
 - On-wafer: contact pad changes
 - Without fully automatic probing, placement repeatability also an issue (10 μm variances common: >2 deg @ 100 GHz)
 - Fixture: DUT placement vs. standards placement... >50 μm variances common

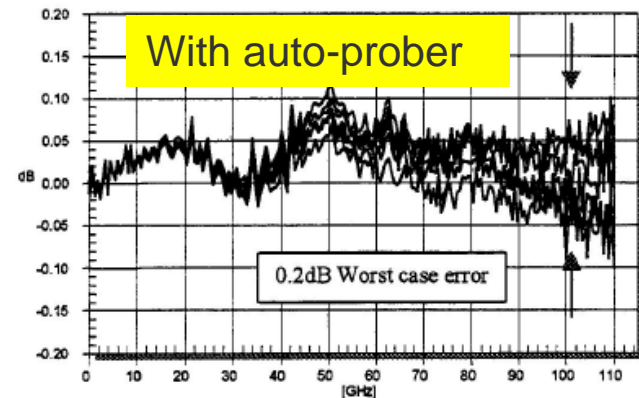


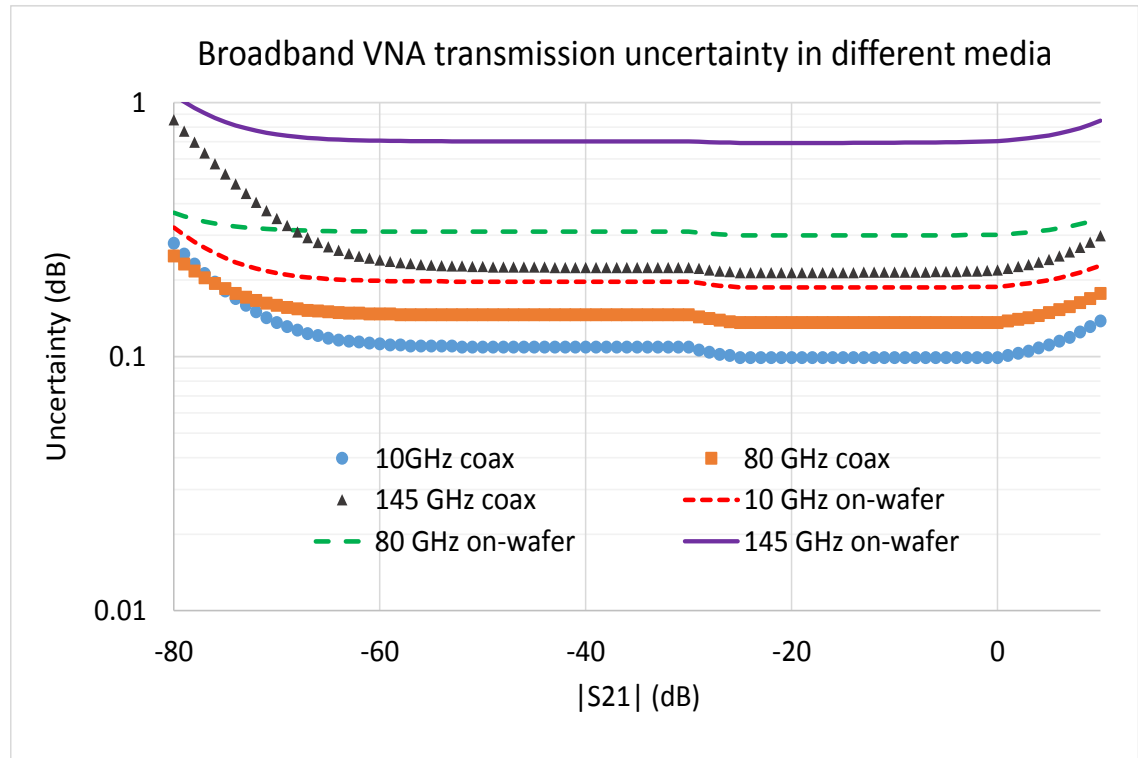
Fig. 14. S_{ii} Open measurement of 8 LRRM calibration using different sets of calibration

From A. Lord, *EuMW Conf. Dig.*, 1999

Mechanisms: Repeatability (2)

- Mid-range transmission uncertainty is often dominated by repeatability-like terms.

- These vary strongly with
 - Frequency,
 - Media, and
 - Condition of the components

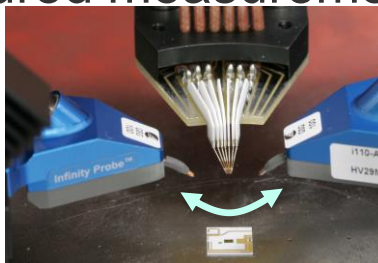


Mechanisms: Repeatability → crosstalk

- Crosstalk internal to instruments generally negligible now.

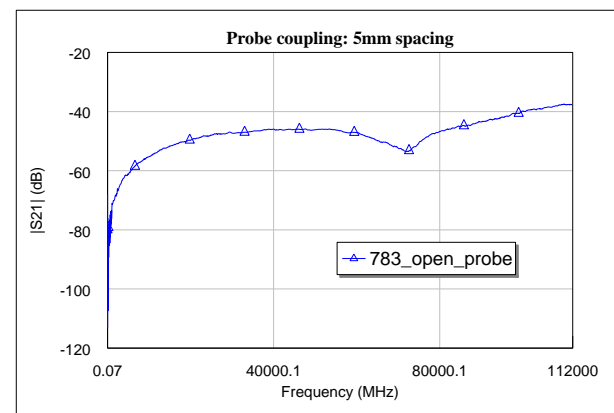
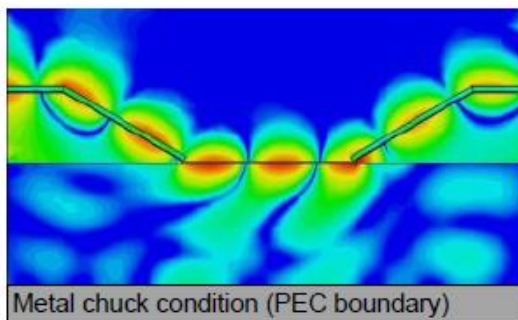
- Coupling in on-wafer and fixtured measurements is not:

- Direct probe-to-probe



- Substrate modes

(energy couples into substrate depending on thickness, chuck details and varies with cal standard/DUT)

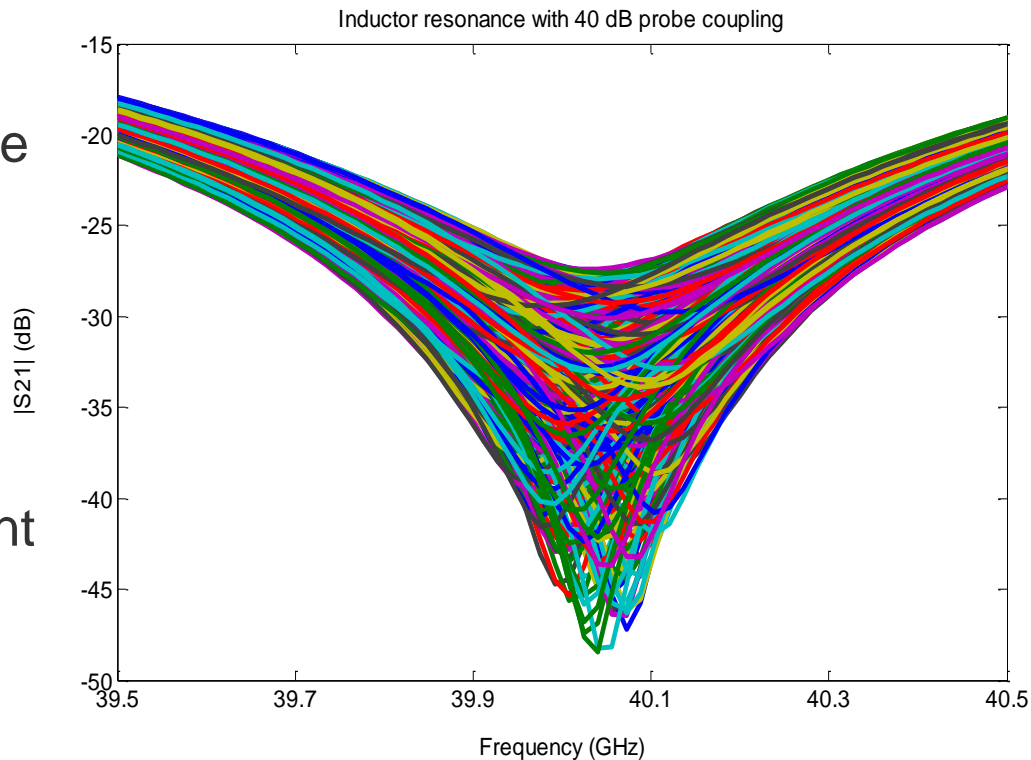


From M. Spirito, et al, 91st
ARFTG Conf. Dig., 2018

- Surface waves

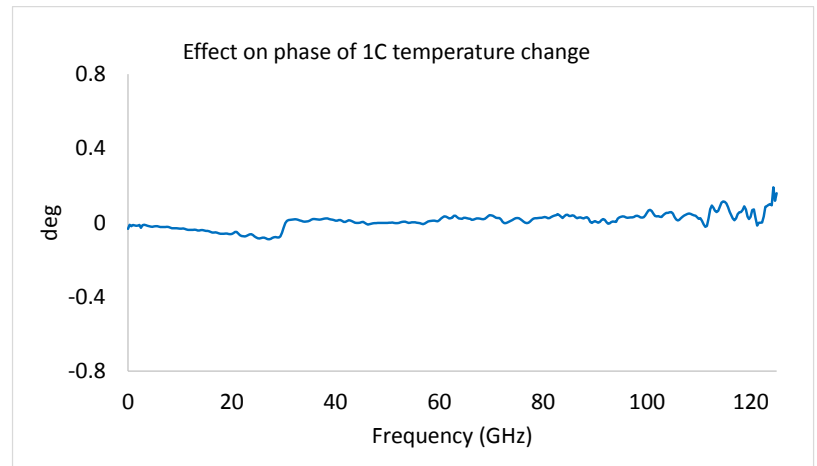
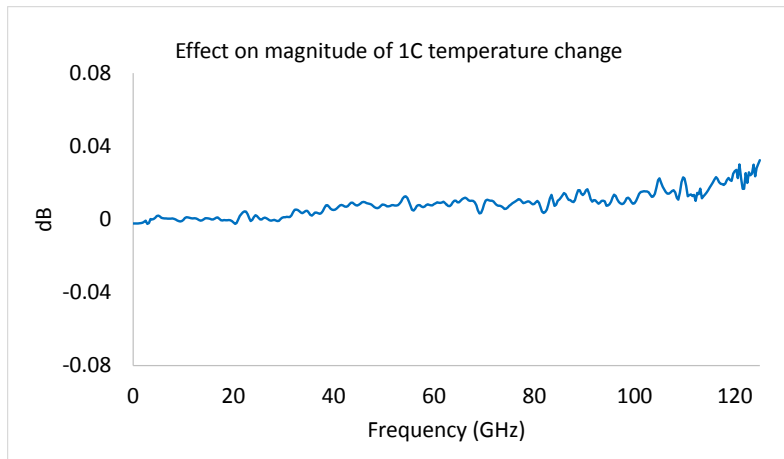
Crosstalk variation and what it can do

- Local resonant frequencies are often used in extraction (e.g., $\frac{1}{\sqrt{LC}}$).
- Depending on the absolute level of the resonant dip, crosstalk variation can obscure the resonant frequency.
- Several % variation in resonant frequency which doubles in component extraction.



Mechanisms: Repeatability → drift

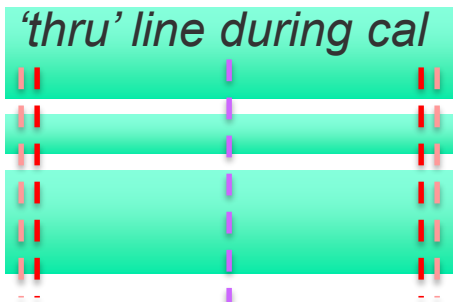
- Setup details (particularly cabling) are very important.
- Magnitude and phase tend to vary at significantly different rates
 - E.g., phase length of coax cables vs. temp
 - Dependent on receiver switching details in some systems



- Since some extractions are dependent on real and imaginary parts of Y- and Z-parameters, this magnitude/phase de-correlation can be important.

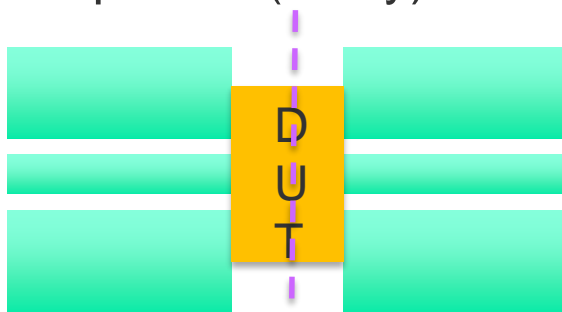
Mechanisms: Calibrations and de-embedding

- A very large topic area...but two recurring themes
 - What assumptions were made?
 - TRL family *strongly* assumes consistent touchdowns/contacts
 - Calibration standards on a different substrate?
 - Some methods require standards (shorts, opens...) to be well-known in advance.
 - Where are the reference planes (really)?

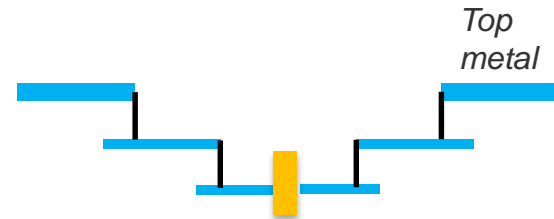


Touchdown where?

Ref plane left in the middle?
envision:ensure



DUT electrical size?
Changes in probe coupling?

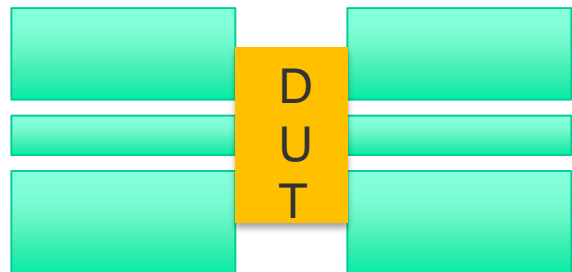
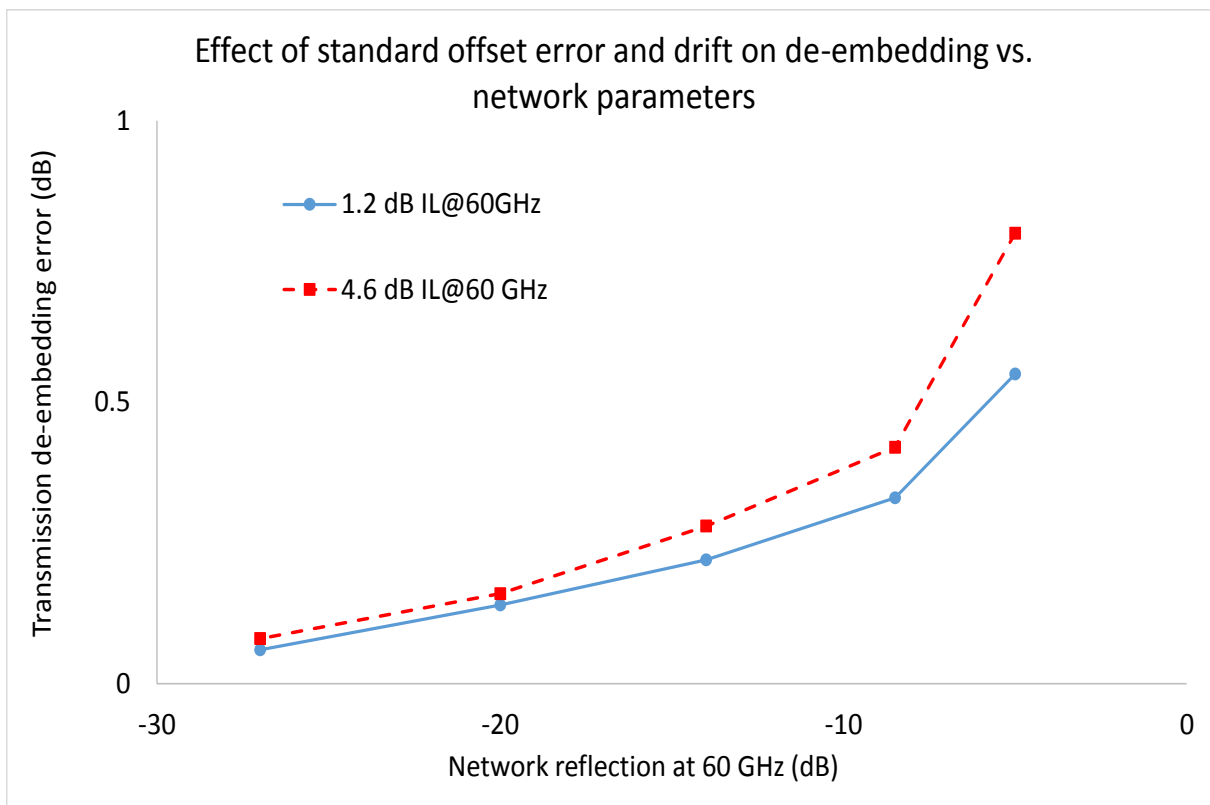


Side view: Many metal layers and via stacks can make the de-embedding more interesting

Calibrations and de-embedding

- Usually, de-embedding a mismatched/lossy network is more sensitive to standards problems and drift.

- The sensitivity gradient is often high for severe mismatches in the network.

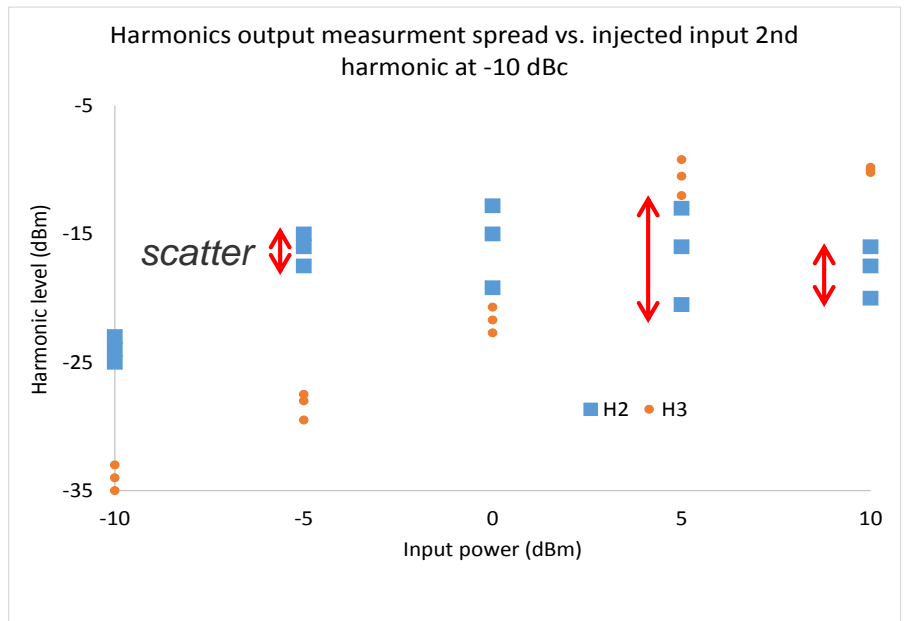
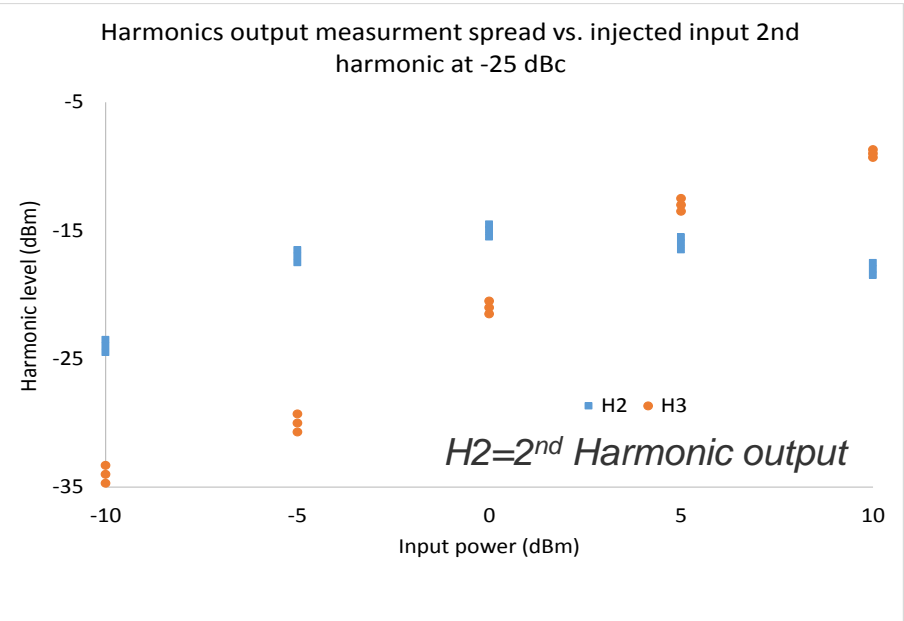


Mechanisms in quasi-linear measurements

- Gain compression, AM-PM conversion, intermodulation distortion, harmonic generation.... can all be useful for model generation.
- Potential added measurement issues:
 - Receiver linearity
 - The receiver had better not be generating the nonlinear products. Shifting signal ranges can help.
 - Source contamination
 - Are extra stimulus signals altering the response?
 - Absolute power
 - How accurate are the drive levels?

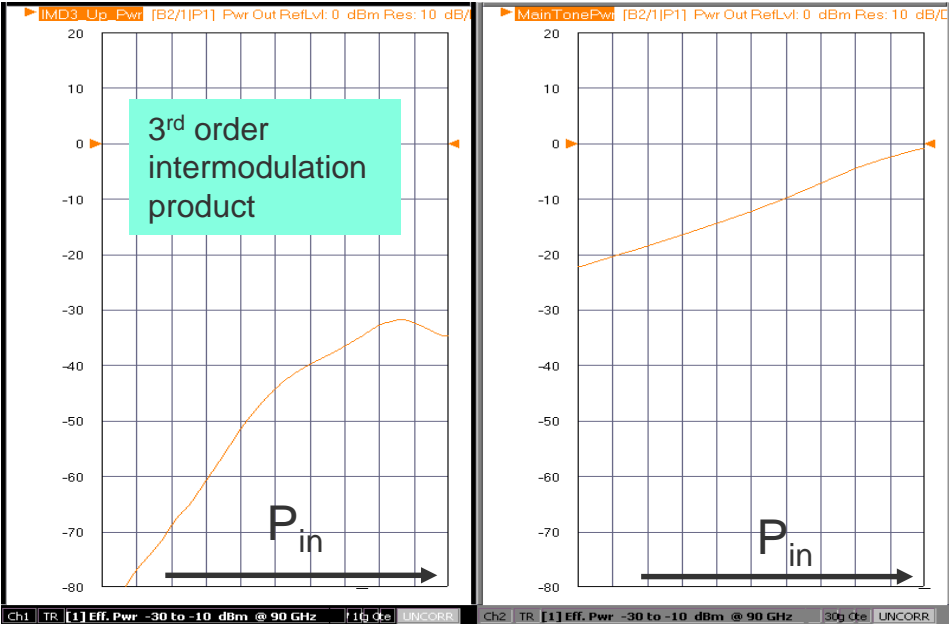
Quasi-linear mechanisms: source harmonics

- An artificial 2nd harmonic was injected at the input with variable phase.
- At high injection levels, the interaction grew dramatically and with variable sensitivity to injection phase.

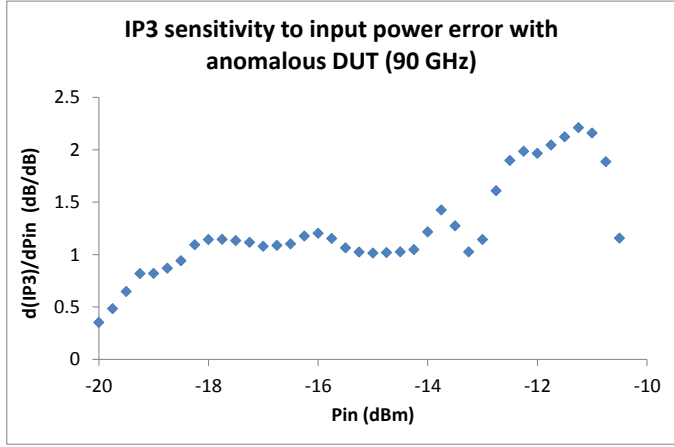


Quasi-linear mechanisms: absolute power

- If the drive level is not known accurately, the main hazard is that the DUT is in a different state than intended.
- The more nonlinear the state, the more it matters...



Some calculated values (e.g., intercept point) can increase sensitivities further!

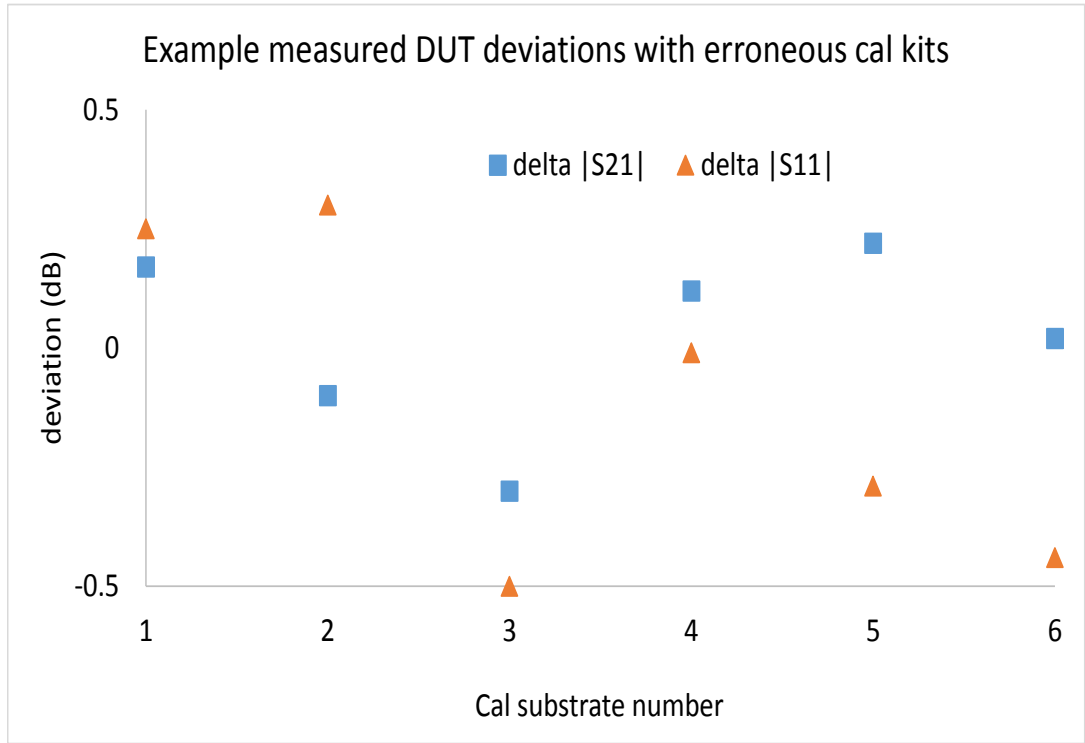


Correlation of uncertainties

- Within an S-parameter
 - Real and imaginary parts could be uncorrelated (e.g., noise dominated)
 - Could be correlated since magnitude and phase have specific behaviors (e.g., drift, some calibration errors)
 - Could be correlated intrinsically (e.g., linearity)
- Between multiple input parameters
 - The S-parameters interact through the calibration/de-embedding so their uncertainties may be correlated
 - Other receivers (e.g., spectrum analyzer) may have uncertainties correlated with the VNA data (e.g., similar linearity issues)

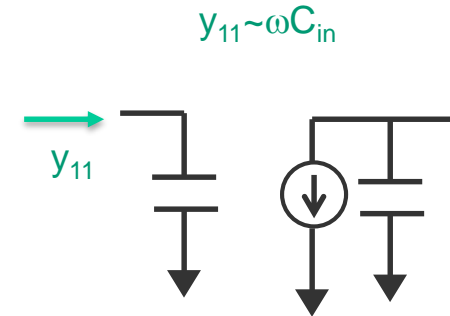
Correlation effects

- The same DUT was measured after calibrating with a series of different (defective) calibration kits.
- Depending on the defect (offset lengths wrong, bad reference impedance...), S_{11} and S_{21} errors may move in the same or different directions.
- ...and we didn't even show phase errors here.



Extraction: compact models

- Y- and Z-parameter conversions are useful since they can pull simple shunt/series circuit elements directly.
- But these transformations are nonlinear in the underlying S-parameters and sensitivities can explode in certain cases.



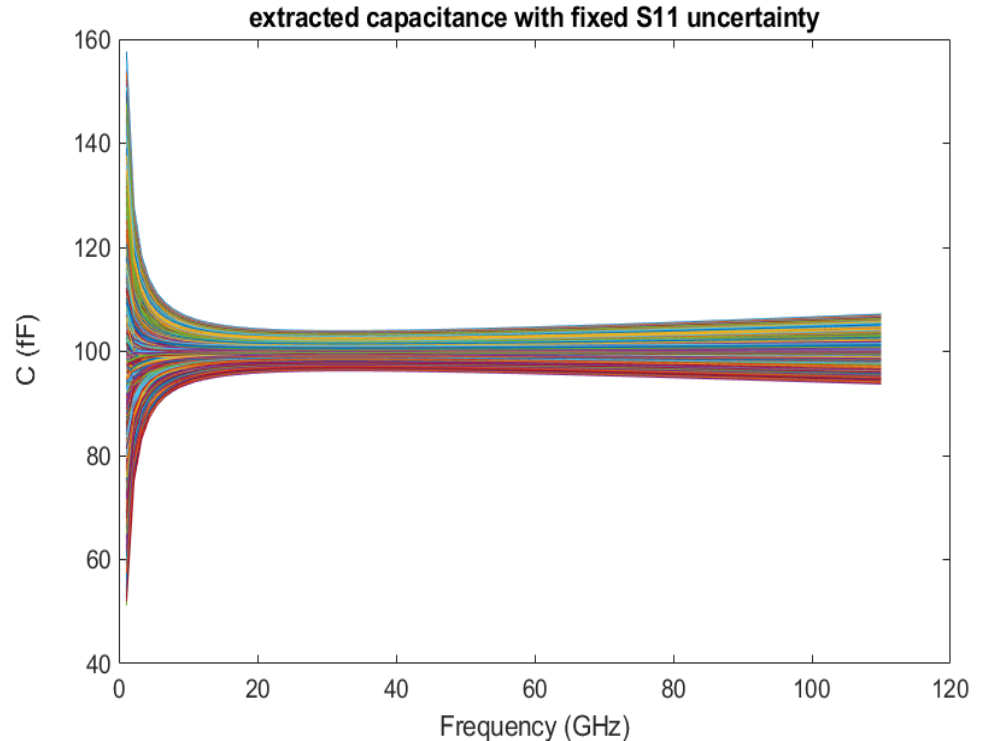
$$y_{11} = \frac{(1 - S_{11})(1 + S_{22}) + 2S_{21}S_{12}}{(1 + S_{11})(1 + S_{22}) - 2S_{21}S_{12}}$$

$$\frac{(\partial y_{11}/y_{11})}{(\partial S_{11}/S_{11})} = \frac{-2S_{11}}{1 - S_{11}^2}$$

Fractional sensitivity gets interesting as $S_{11} \rightarrow$ open or short.

Extraction example: Monte Carlo uncertainties

- Even if the underlying S-parameter uncertainty was constant with frequency, the capacitance uncertainty has structure.
- In practice, reflection uncertainty is fairly constant at modest- to high-reflection levels so this approximation is ~realistic.

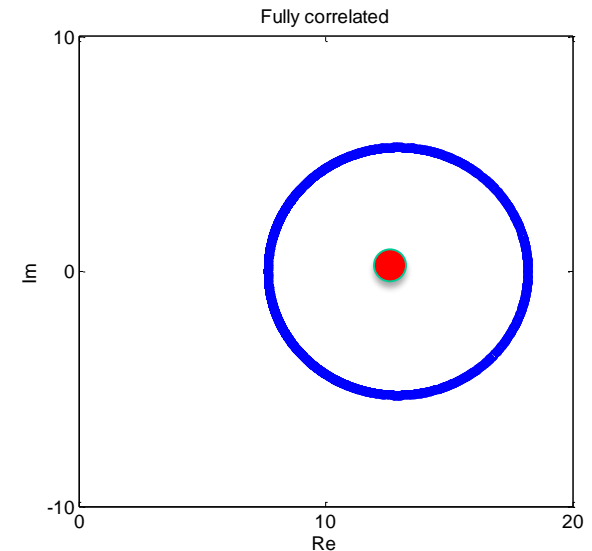
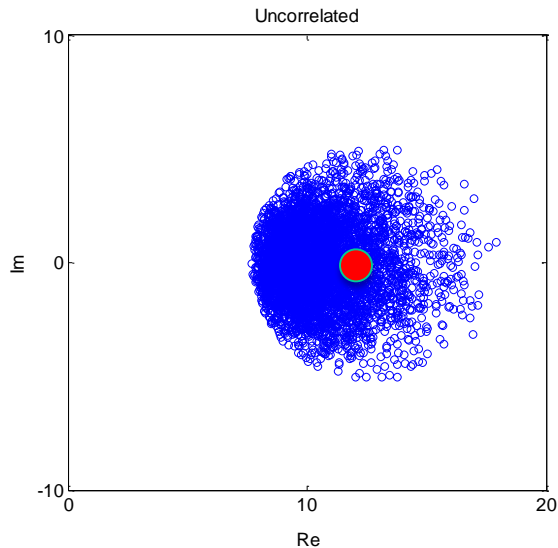


Extractions and correlation

$$Z_{21} = \frac{2S_{21}}{(1 - S_{11})(1 - S_{22}) - 2S_{21}S_{12}}$$

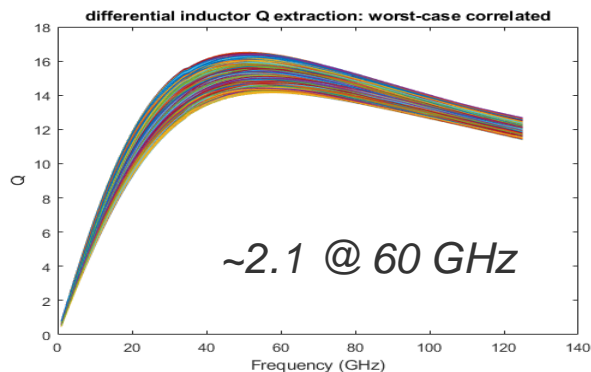
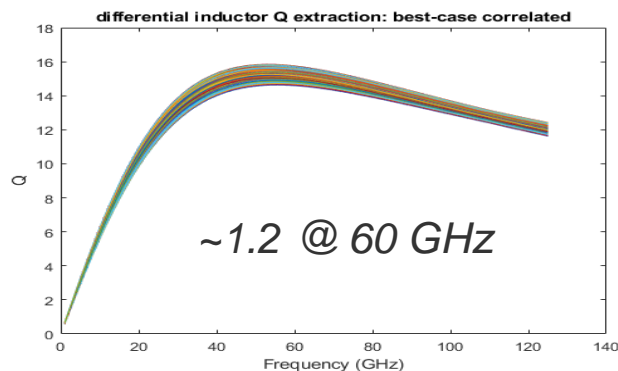
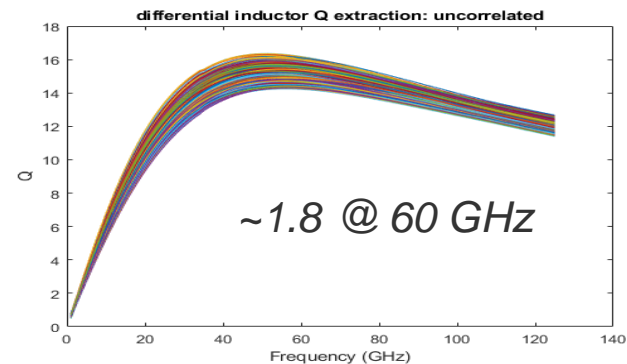
- Even the simplest component extraction (e.g., a series inductor) might involve multiple S-parameters. How are those uncertainties correlated?

If drift/linearity dominates, the terms may be highly correlated and the distribution of uncertainty would be less favorable.



Extraction example: inductor Q

- Inductor Q ($Im(1/Y_{12})/Re(1/Y_{12})$) makes use of several S-parameters. How those uncertainties are correlated can significantly affect the Q uncertainty.

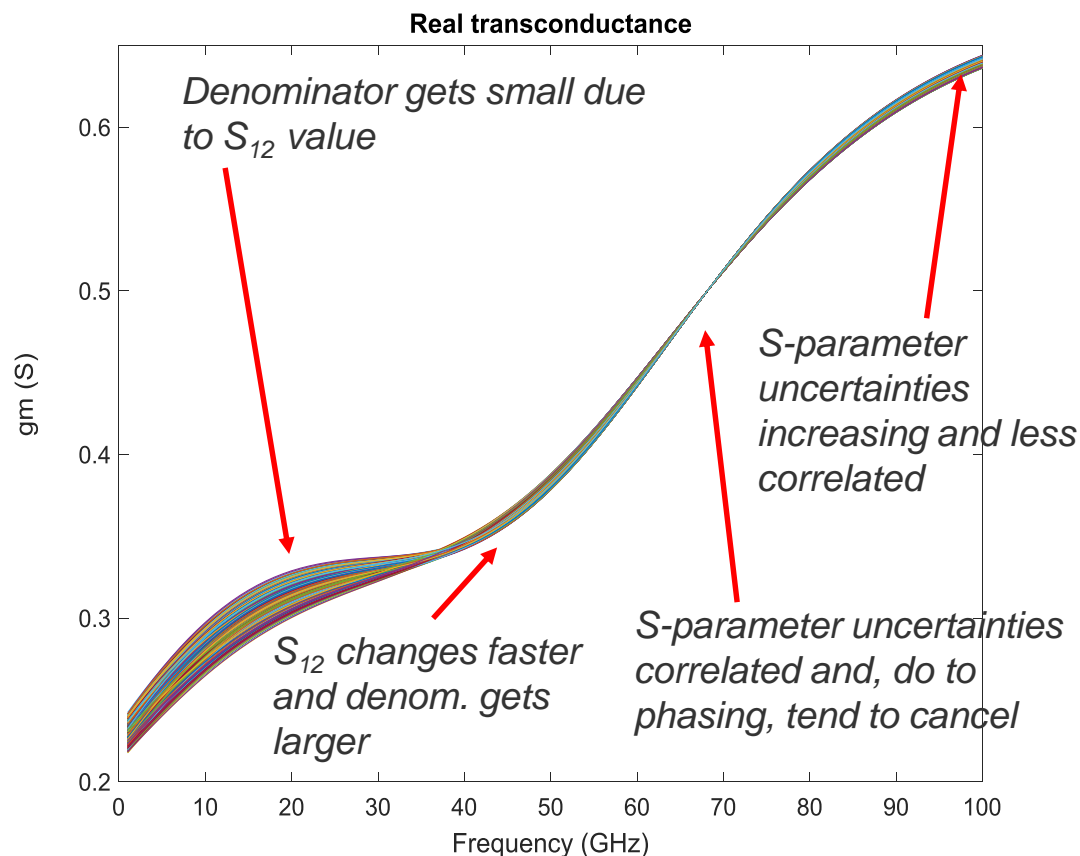


- Level of correlation affected by the measurement hardware choice, the parameter space, and the calibration/de-embedding choices.

Extraction example (3)

- Sometimes high frequency transconductance is extracted directly (rather than low freq. I-V data + high freq. parasitics).
- $\text{Re}(Y_{21})$ can be used but S-parameter uncertainty are usually mag/phase local so interesting conversions happen.

$$y_{21} = \frac{-2S_{21}}{(1 + S_{11})(1 + S_{22}) - 2S_{21}S_{12}}$$

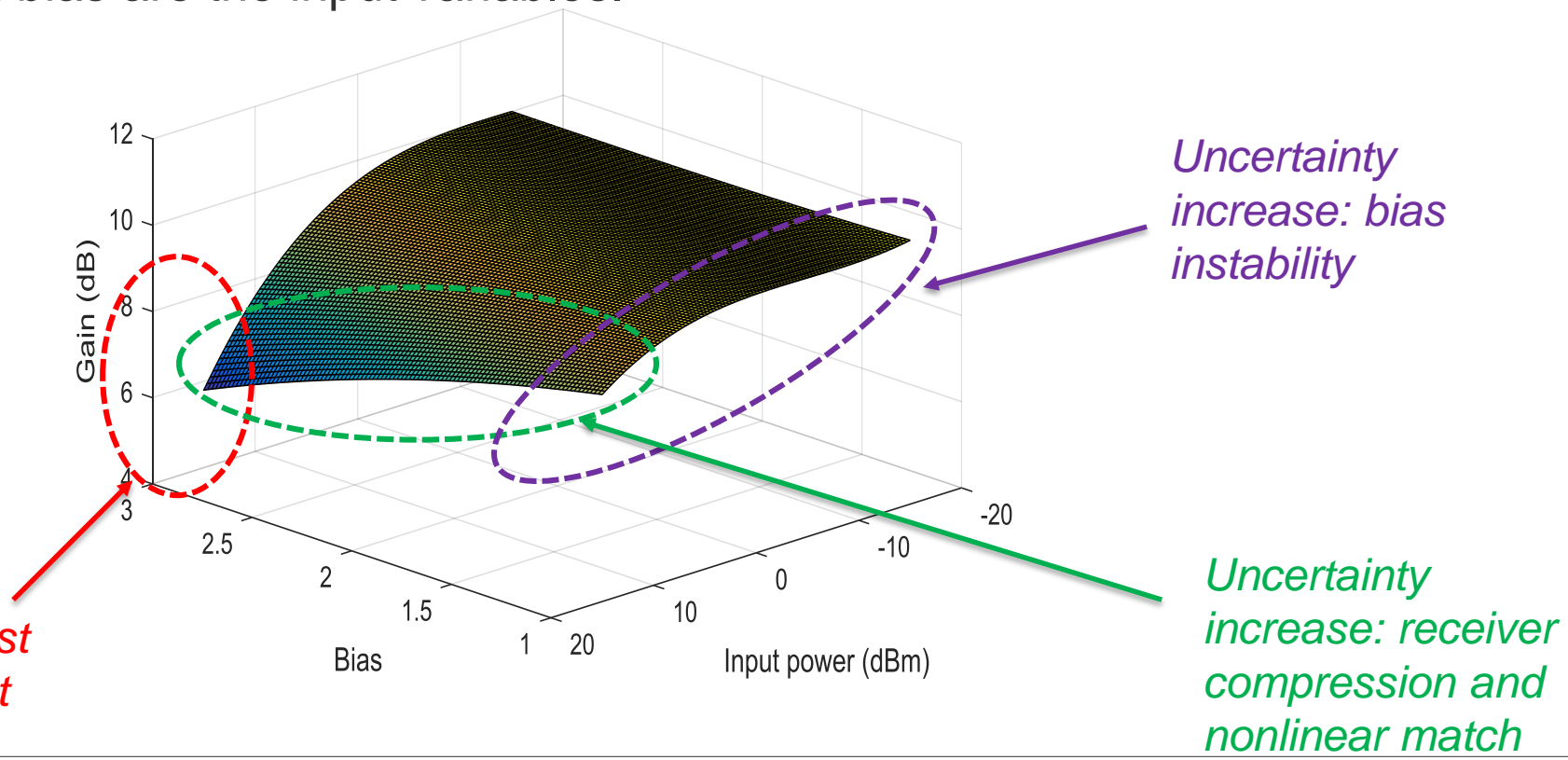


Behavioral models

- A black-box approach to modeling acquires parameters over frequency, power, bias, etc. and then uses that database (along with interpolation and extrapolation) to predict behavior elsewhere.
- How much data should be collected?
- How should interpolation and extrapolation be done?
- How do we fold in uncertainty knowledge over the response surface?

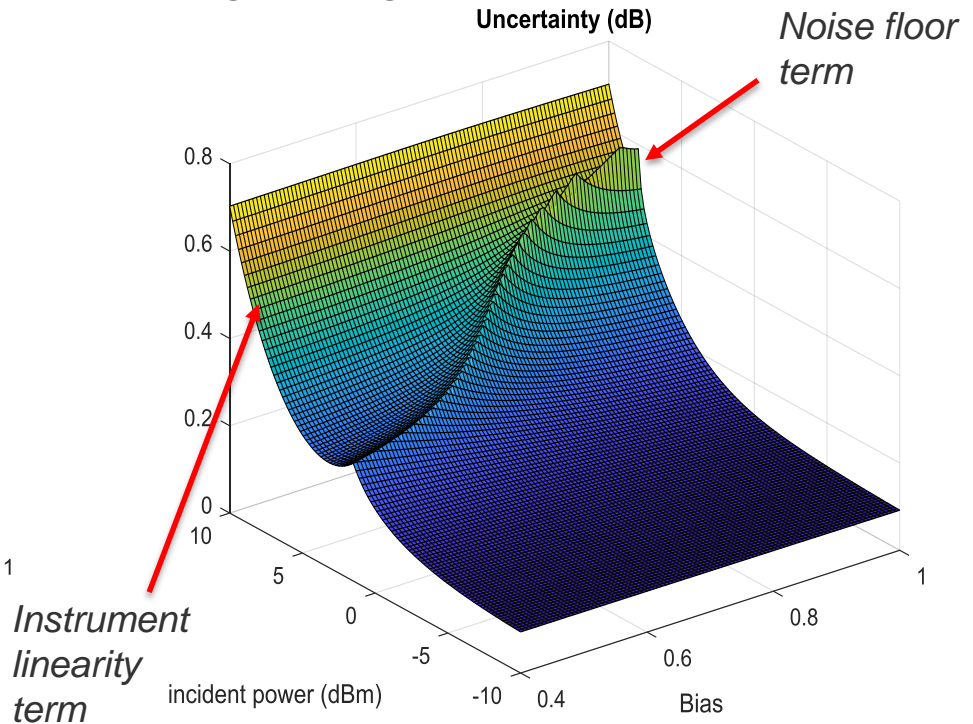
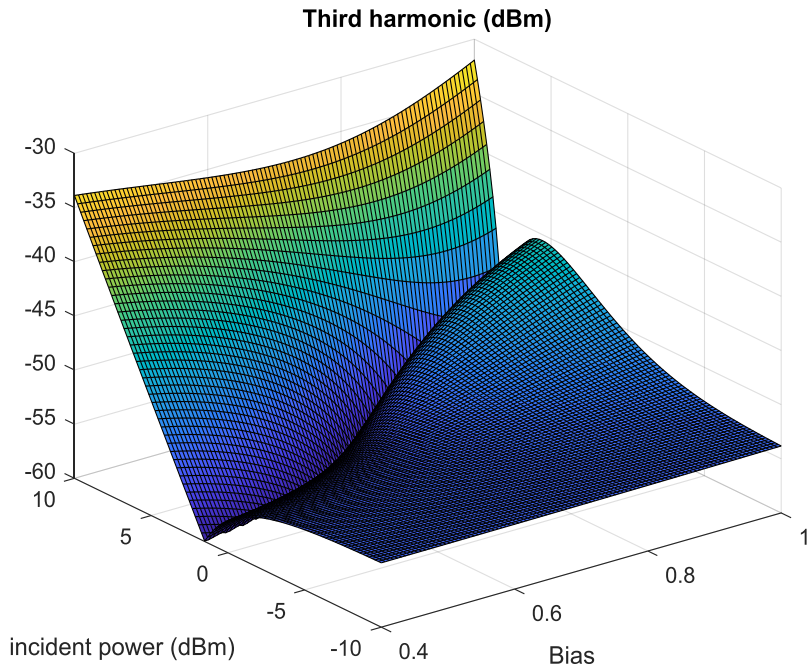
Behavioral models (2)

- A simple gain compression problem is sketched below where drive power and bias are the input variables.



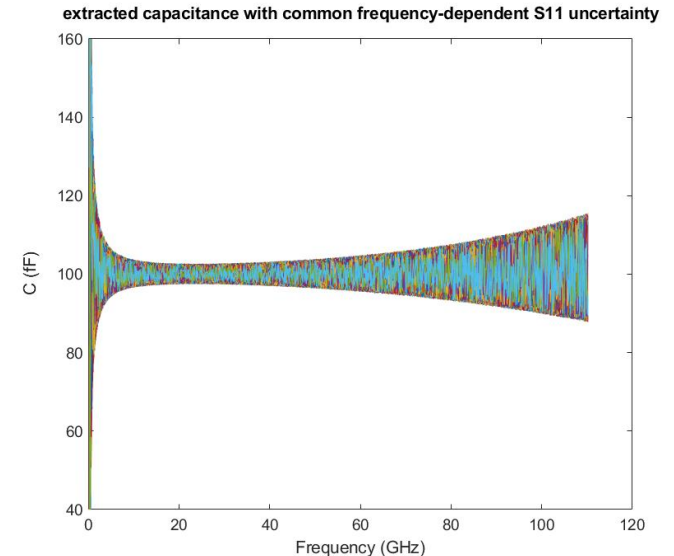
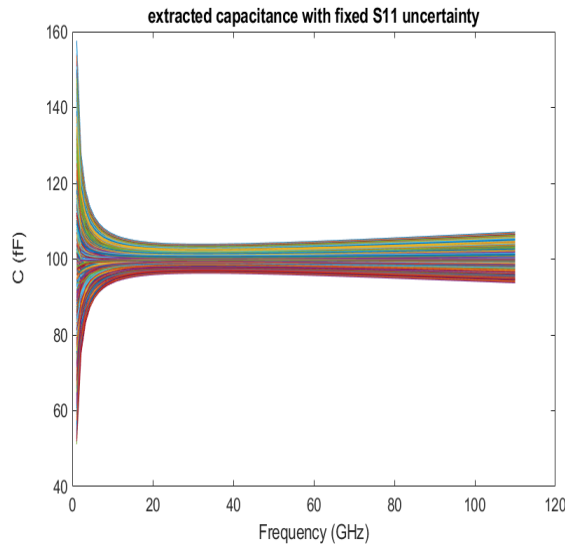
Behavioral model example

- Interpolating/extrapolating on a complex surface can be a challenge and uncertainties may be moving differently.
- Measurement hardware configuration changes might help.



Uncertainty and sensitivity overlap

- Going back to the capacitor example with realistic uncertainties, the picture changes.
- Extreme frequencies have higher (usually) uncertainties which is where the sensitivities increase as well. Extrapolation-based processes can be impacted.

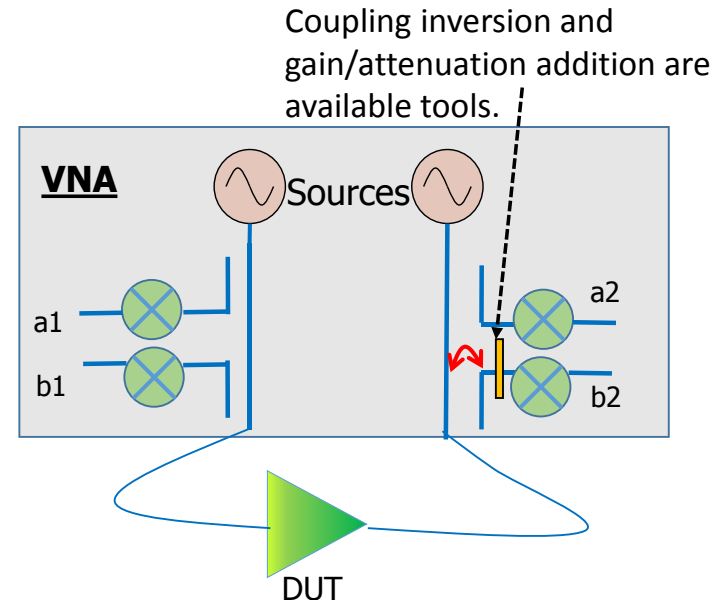


Some mitigation strategies

- Some care may be needed when asymptotic or extrapolated values are of interest.
- Optimize the signal level, when free to do so, to improve uncertainties.
- Choose calibration/de-embedding processes that do not add correlation where it would be problematic. (*don't always know in advance...*)
- Measurement hardware choices: may affect uncertainty directly or may change correlation levels.

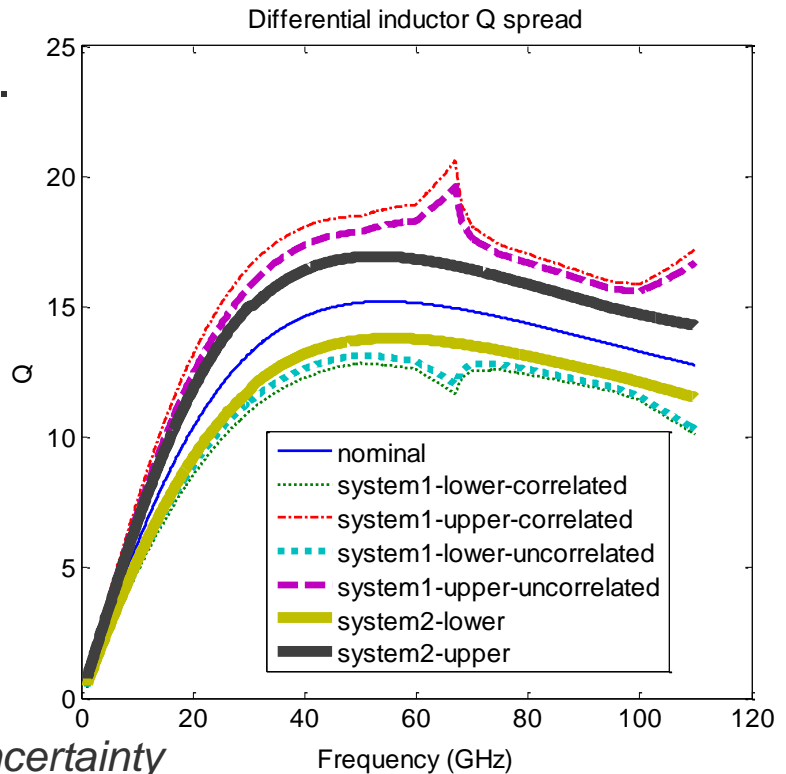
Mitigation strategies: signal level control

- Passive devices:
 - Generally increasing drive level to near the point of trace noise-compression crossover can help
- Active Devices:
 - May be a cap on the drive level to ensure DUT linearity (dynamic range challenge: additive noise)
 - Receiver sensitivities can sometimes be altered (signal path changes, attenuation choices)
- Other measurement parameters that may be relevant: measurement bandwidth (of course), synthesis modes (that can affect phase noise)...



Mitigation strategies: correlation control

- Some hardware uncertainty terms (drift and linearity) foster more correlation between parameters than others (noise).
- Certain calibration/de-embedding approaches also more tightly correlate individual parameters (TRL family more so than defined-standard family).

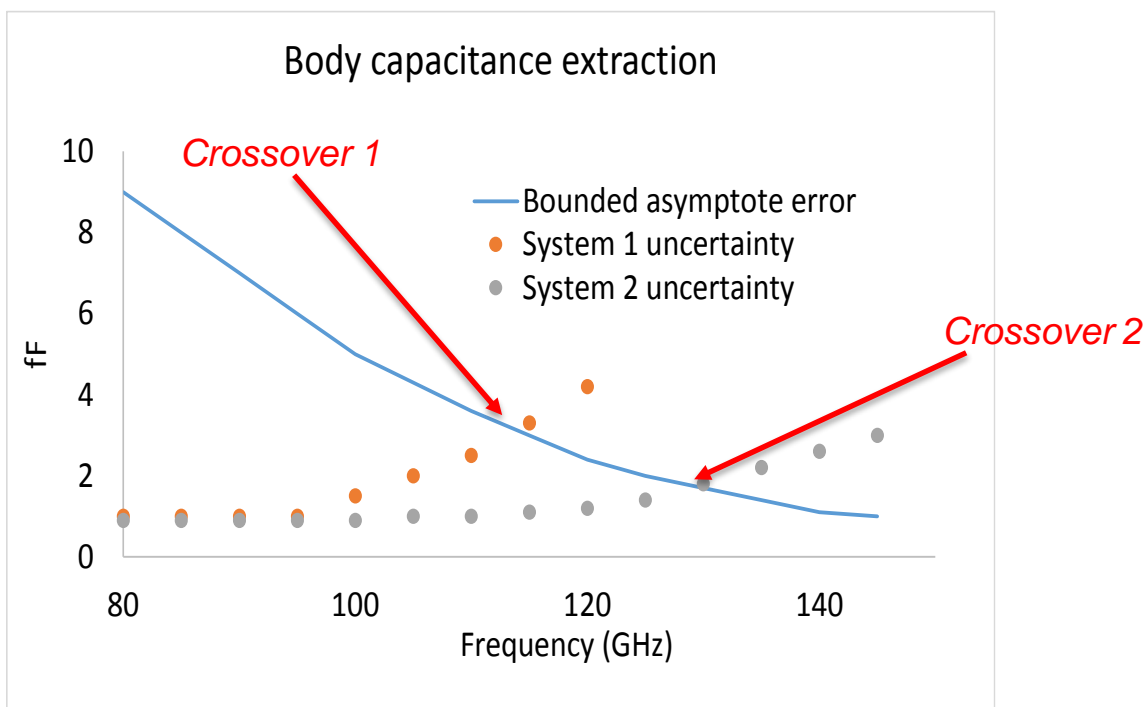


System 1 uncertainty was drift-dominated. System 2 uncertainty was noise-dominated and correlation had little effect.

Mitigation strategies: Asymptotic analysis

- Some extractions rely on 'high' or 'low' frequency data so other parasitics can be neglected.

- The measurement uncertainties might increase at those limits. Make a decision on what data to use.



Summary

- Many different model extraction techniques are popular and all interact with underlying data uncertainties in different ways.
- Mm-wave measurements are generally more challenging to begin with so the uncertainties may play a greater role.
- Quantifying those uncertainty mechanisms is somewhat easier than in the past and allows a better exploration of the parameter spaces and can improve model extraction.